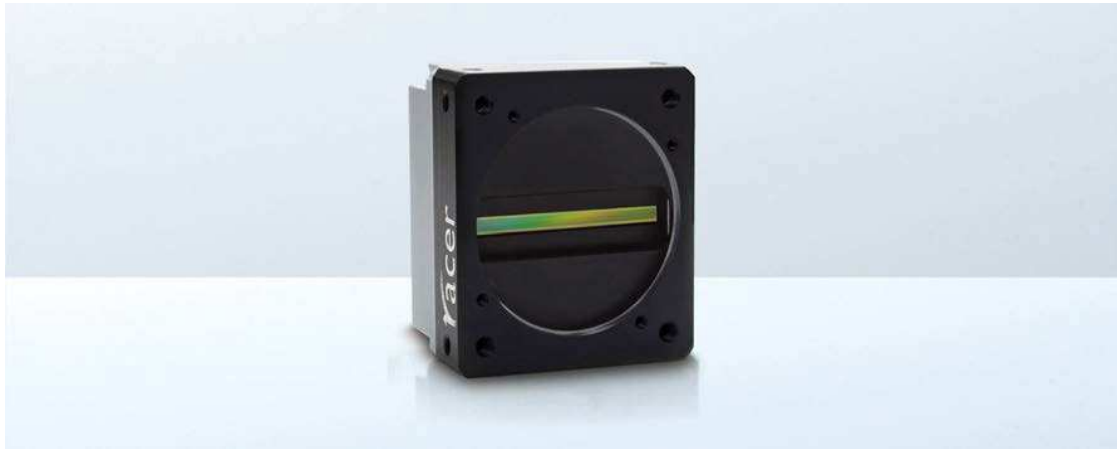


Basler raL6144-80km



Camera Specification

Measurement protocol using the EMVA Standard 1288

Document Number: BD000798

Version: 01



For customers in the U.S.A.

This equipment has been tested and found to comply with the limits for a Class A digital device, pursuant to Part 15 of the FCC Rules. These limits are designed to provide reasonable protection against harmful interference when the equipment is operated in a commercial environment. This equipment generates, uses, and can radiate radio frequency energy and, if not installed and used in accordance with the instruction manual, may cause harmful interference to radio communications. Operation of this equipment in a residential area is likely to cause harmful interference in which case the user will be required to correct the interference at his own expense.

You are cautioned that any changes or modifications not expressly approved in this manual could void your authority to operate this equipment.

The shielded interface cable recommended in this manual must be used with this equipment in order to comply with the limits for a computing device pursuant to Subpart J of Part 15 of FCC Rules.

For customers in Canada

This apparatus complies with the Class A limits for radio noise emissions set out in Radio Interference Regulations.

Pour utilisateurs au Canada

Cet appareil est conforme aux normes Classe A pour bruits radioélectriques, spécifiées dans le Règlement sur le brouillage radioélectrique.

Life Support Applications

These products are not designed for use in life support appliances, devices, or systems where malfunction of these products can reasonably be expected to result in personal injury. Basler customers using or selling these products for use in such applications do so at their own risk and agree to fully indemnify Basler for any damages resulting from such improper use or sale.

Warranty Note

Do not open the housing of the camera. The warranty becomes void if the housing is opened.

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1 Overview

Basler raL6144-80km				
Item	Symbol	Typ. ⁽¹⁾	Unit	Remarks
Temporal Noise Parameters				
Total Quantum Efficiency (QE)	η	41 ⁽²⁾	%	$\lambda = 545 \text{ nm}$
Inverse of Overall System Gain	$\frac{1}{K}$	6.3	$\frac{e^-}{DN}$	
Temporal Dark Noise	σ_{do}	8	e^-	
Saturation Capacity	$\mu_{e.sat}$	25600	e^-	
Derived Parameters				
Absolute Sensitivity Threshold	$\mu_{p.min}$	20	$p\sim$	$\lambda = 545 \text{ nm}$
Dynamic Range	$DYN_{out.bit}$	11.6	bit	
Maximum SNR	$SNR_{y.max.bit}$	7.3	bit	
	$SNR_{y.max.dB}$	44.1	dB	
Item	Symbol	Typ.	Unit	Remarks
Spatial Noise Parameters				
Spatial Offset Noise, $DSNU_{1288}$	σ_o	4.0	e^-	
Spatial Gain Noise, $PRNU_{1288}$	S_g	0.2 ⁽²⁾	%	

Table 1: Most Important Specification Data

Operating Point		
Item	Symbol	Remarks
Video output format		12 bits/pixel(Mono16)
Gain	Register raw	256
Offset	Register raw	32
Exposure time	T_{exp}	2.0 μs to 3.8 ms

Table 2: Operating Point for the Camera Used

⁽¹⁾ The unit e^- is used in this document as a statistically measured quantity.

⁽²⁾ See appendix "Deviation in Quantum Efficiency" and "Photo Response Non Uniformity".

2 Introduction

This measurement protocol describes the specification of Basler raL6144-80km cameras. The measurement methods conform to the 1288 EMVA Standard, the Standard for Characterization and Presentation of Specification Data for Image Sensors and Cameras (Release A1.03) of the European Machine Vision Association (EMVA) [1].

The most important specification data for Basler raL6144-80km cameras is summarized in table 1.

3 Basic Information

Basic Information	
Vendor	Basler
Model	raL6144-80km
Type of data presented	Typical
Number of samples	33
Sensor	Awaiba DR-6k-7 Linear
Sensor type	CMOS
Sensor diagonal	
Indication of lens category to be used	F-Mount
Resolution	6144 pixel
Pixel width	7.00 μm
Pixel height	7.00 μm
Readout type	
Transfer type	
Shutter type	-
Overlap capabilities	
Maximum readout rate	80.0 kHz
General conventions	-
Interface type	Camera Link

Table 3: Basic Information

3.1 Illumination

3.1.1 Illumination Setup for the Basler Camera Test Tool

The illumination during the testing on each camera was fixed. The drift in the illumination over a long period of time and after the lamp is changed is measured by a reference Basler A602fc camera. The reference camera provides an intensity factor that was used to calculate the irradiance for each camera measurement.

Light Source				
Item	Symbol	Typ.	Unit	Remarks
Wavelength	λ	545	nm	
Wavelength Variation	$\Delta\lambda$	50	nm	
Distance sensor to light source	d	280	mm	
Diameter of the light source	D	35	mm	
f-Number	$f_{\#}$	8		$f_{\#} = \frac{d}{D}$

Table 4: Light Source

3.1.2 Measurement of the Irradiance

The irradiance was measured using an IL1700 Radiometer from International Light Inc. (Detector: SEL033 #6285; Input optic: W #9461; Filter: F #21487; regular calibration). The accuracy of the Radiometer is specified as $\pm 3.5\%$.

The measured irradiance is plotted in figure 1.

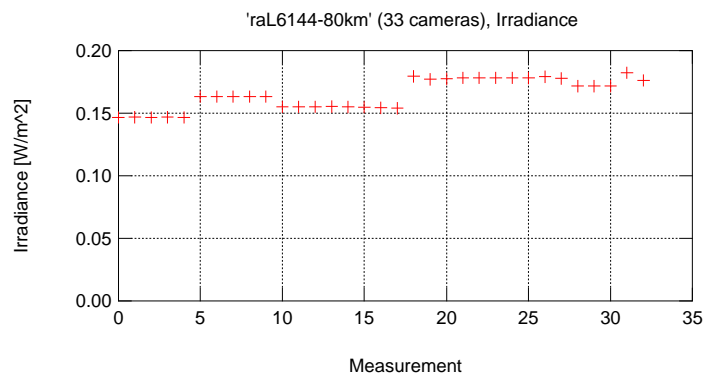


Figure 1: Irradiance for Each Camera Measurement

The error for each calculated value using the amount of light falling on the sensor is dependent on the accuracy of the irradiance measurement.

4 Characterizing Temporal Noise and Sensitivity

4.1 Basic Parameters

4.1.1 Total Quantum Efficiency ⁽³⁾

Total Quantum Efficiency for One Fixed Wavelength Total quantum efficiency $\eta(\lambda)$ in [%] for monochrome light at $\lambda = 545$ nm with a wavelength variation of $\Delta\lambda = 50$ nm.

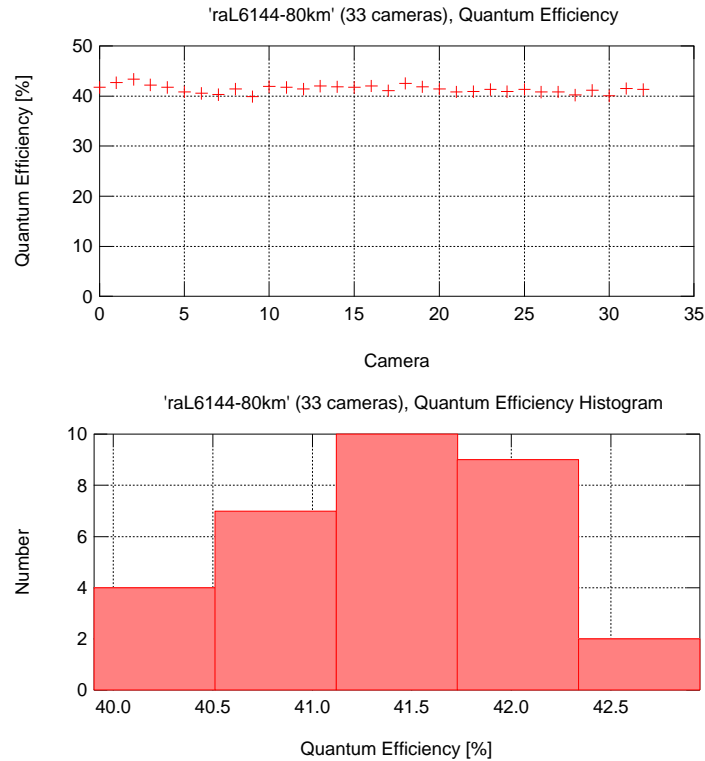


Figure 2: Total Quantum Efficiency (QE)

Item	Symbol	Typ.	Std. Dev.	Unit	Remarks
Total Quantum Efficiency (QE)	η	41	TBD	%	$\lambda = 545$ nm

Table 5: Total Quantum Efficiency (QE)

The main error in the total quantum efficiency $\Delta\eta$ is related to the error in the measurement of the illumination as described in section 3.1.

⁽³⁾ See appendix "Deviation in Quantum Efficiency" and "Photo Response Non Uniformity".

Total Quantum Efficiency Versus Wavelength of the Light Total quantum efficiency $\eta(\lambda)$ in [%] for monochrome light versus wavelength of the light in [nm] .
See appendix "Deviation in Quantum Efficiency" and "Photo Response Non Uniformity".

4.1.2 Temporal Dark Noise

Standard deviation of the temporal dark noise σ_{d_0} referenced to electrons for exposure time zero in $[e^-]$.

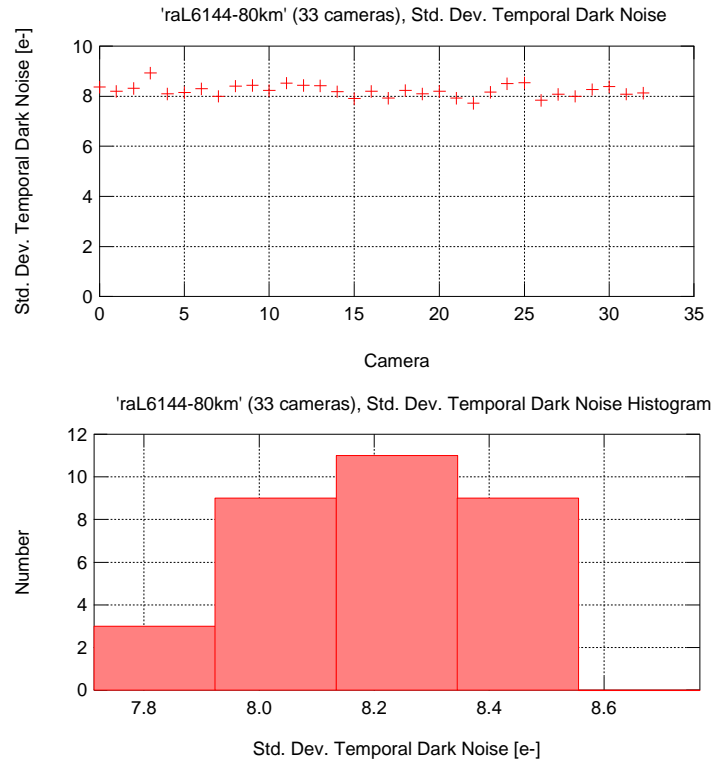


Figure 3: Temporal Dark Noise

Item	Symbol	Typ.	Std. Dev.	Unit	Remarks
Temporal Dark Noise	σ_{d_0}	8	0.2	e^-	

Table 6: Temporal Dark Noise

4.1.3 Dark Current

Dark current N_{d30} for a housing temperature of 30° C in $[e^-/s]$.
Not measured!

4.1.4 Doubling Temperature

Doubling temperature k_d of the dark current in $[°\text{C}]$.
Not measured!

4.1.5 Inverse of Overall System Gain

Inverse of overall system gain $\frac{1}{K}$ in $[\frac{e^-}{DN}]$.

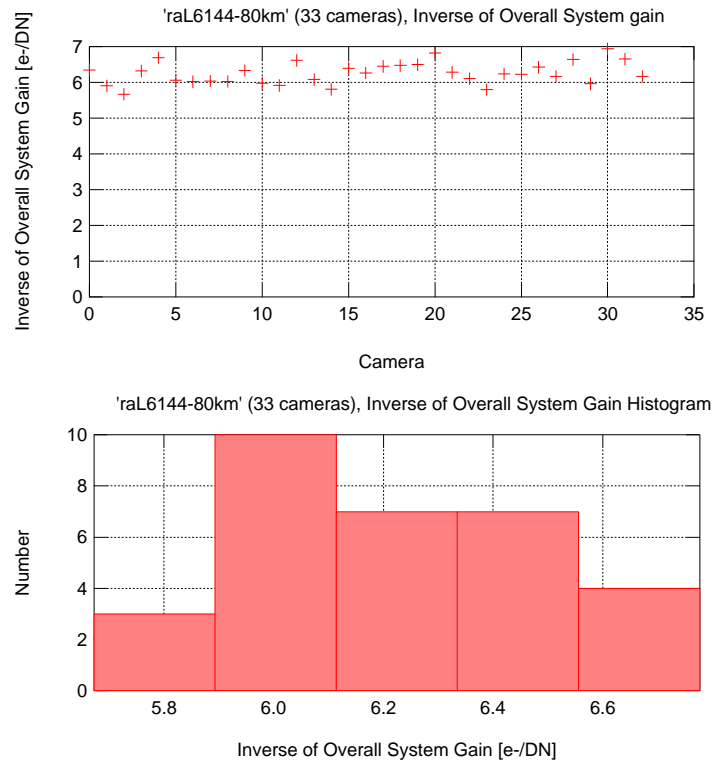


Figure 4: Inverse of Overall System Gain

Item	Symbol	Typ.	Std. Dev.	Unit	Remarks
Inverse of Overall System Gain	$\frac{1}{K}$	6.3	0.31	$\frac{e^-}{DN}$	

Table 7: Inverse of Overall System Gain

4.1.6 Inverse Photon Transfer

Inverse photon transfer $\frac{1}{\eta K}$ in $\left[\frac{p \sim}{DN} \right]$.

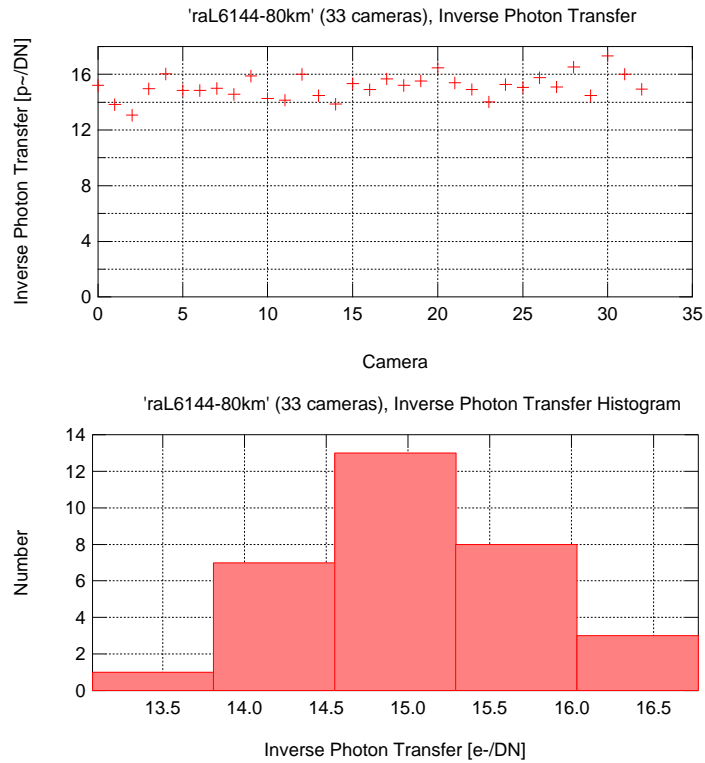


Figure 5: Inverse Photon Transfer

Item	Symbol	Typ.	Std. Dev.	Unit	Remarks
Inverse Photon Transfer	$\frac{1}{\eta K}$	15.1	TBD	$\frac{p \sim}{DN}$	$\lambda = 545 \text{ nm}$

Table 8: Inverse Photon Transfer

The main error in the inverse photon transfer $\frac{1}{\eta K}$ is related to the error in the measurement of the illumination as described in section 3.1.

4.1.7 Saturation Capacity

Saturation capacity $\mu_{e.sat}$ referenced to electrons in $[e^-]$.

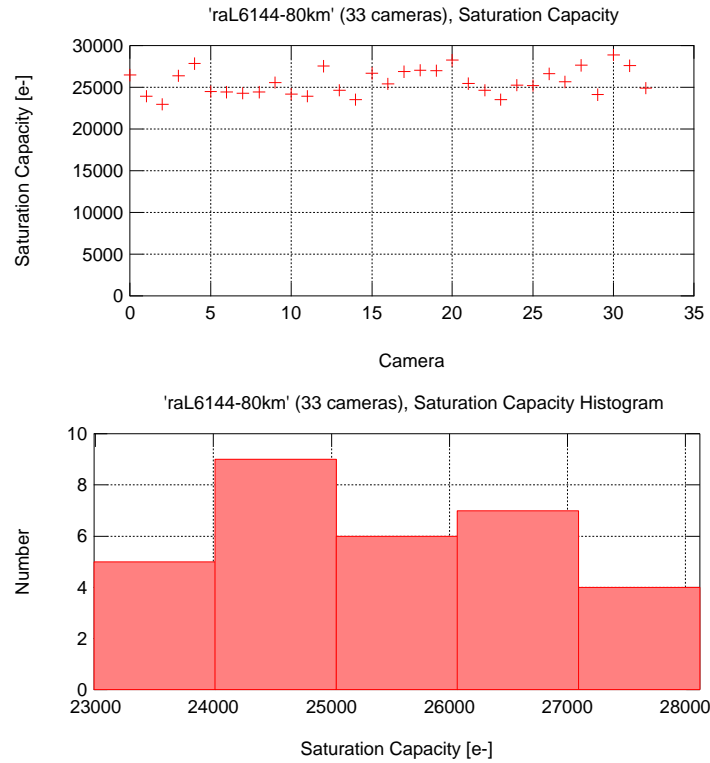


Figure 6: Saturation Capacity

Item	Symbol	Typ.	Std. Dev.	Unit	Remarks
Saturation Capacity	$\mu_{e.sat}$	25600	1550	e^-	

Table 9: Saturation Capacity

4.2 Derived Data

4.2.1 Absolute Sensitivity Threshold

Absolute sensitivity threshold $\mu_{p.min}(\lambda)$ in $[p\sim]$ for monochrome light versus wavelength of the light in $[nm]$.

$$\mu_{p.min} = \frac{\sigma_{d_0}}{\eta} \tag{1}$$

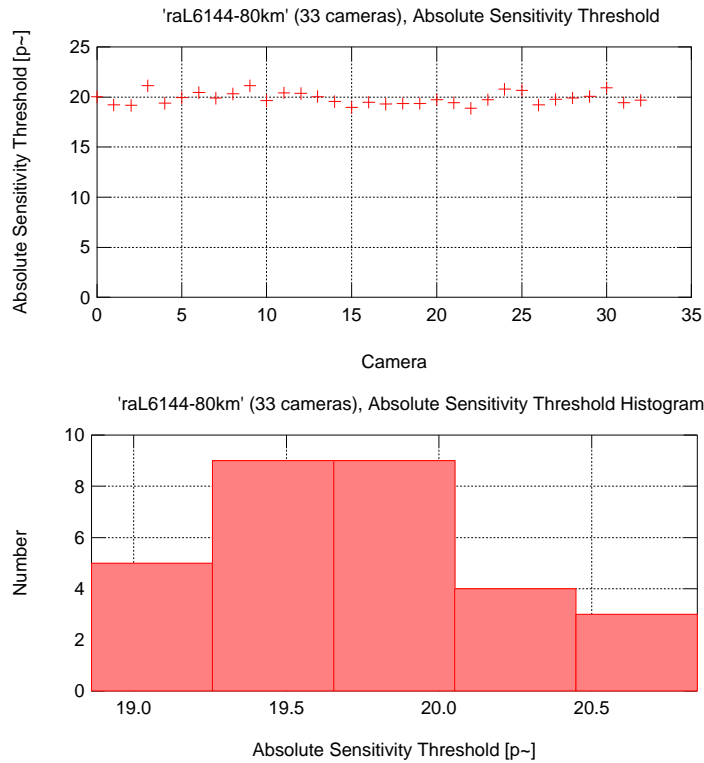


Figure 7: Absolute Sensitivity Threshold

Item	Symbol	Typ.	Std. Dev.	Unit	Remarks
Absolute Sensitivity Threshold	$\mu_{p.min}$	20	TBD	$p\sim$	$\lambda = 545 \text{ nm}$

Table 10: Absolute Sensitivity Threshold

4.2.2 Signal-to-noise Ratio

Signal-to-noise ratio $\text{SNR}_y(\mu_p)$ is plotted versus number of photons μ_p collected in a pixel during exposure time in $[\text{p}^\sim]$ for monochrome light with the wavelength λ given in $[\text{nm}]$. The wavelength should be near the maximum of the quantum efficiency.

$$A : \text{SNR}_y = \frac{\mu_y - \mu_{y,\text{dark}}}{\sigma_y} \quad (2)$$

$$B : \text{SNR}_y = \frac{\eta\mu_p}{\sqrt{(\eta\mu_p + \sigma_{d_0}^2)}} \quad (3)$$

Figure 8 shows the signal-to-noise ratio SNR_y for monochrome light with the wavelength $\lambda = 545 \text{ nm}$.

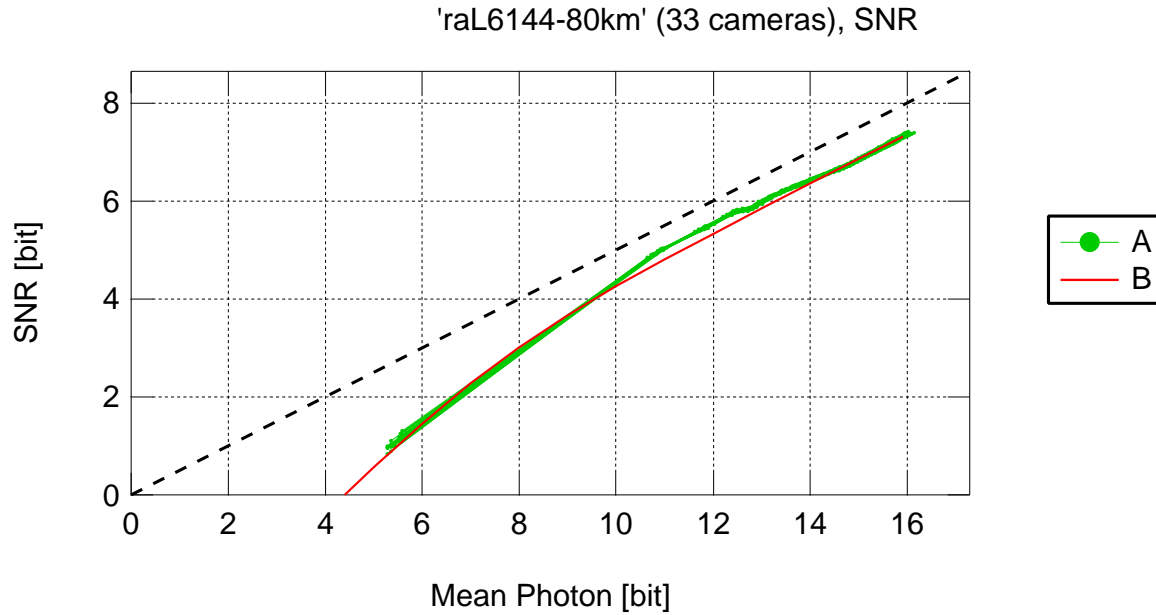


Figure 8: Signal-to-noise Ratio

The maximum achievable image quality is given as $\text{SNR}_{y,\text{max}}$.

$$\text{SNR}_{y,\text{max}} = \sqrt{\mu_{e,\text{sat}}} \quad (4)$$

$$\text{SNR}_{y,\text{max},\text{bit}} = \text{ld } \text{SNR}_{y,\text{max}} = \frac{\log \text{SNR}_{y,\text{max}}}{\log 2} \quad (5)$$

$$\text{SNR}_{y,\text{max},\text{dB}} = 20 \log \text{SNR}_{y,\text{max}} \approx 6.02 \text{SNR}_{y,\text{max},\text{bit}} \quad (6)$$

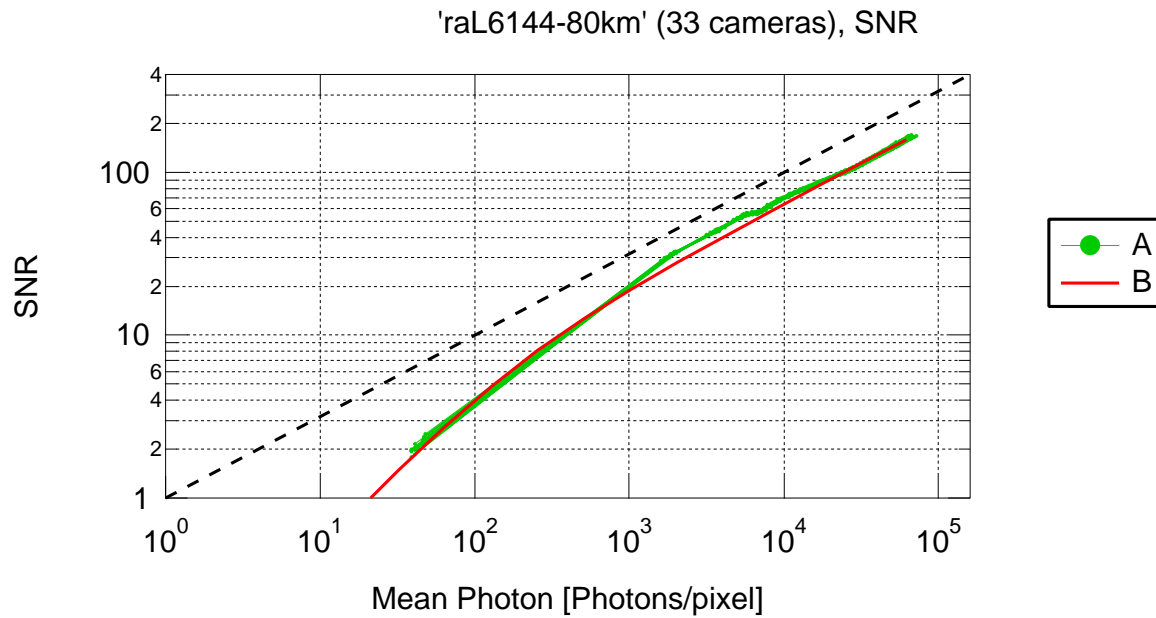


Figure 9: Signal-to-noise Ratio

Item	Symbol	Typ.	Std. Dev.	Unit	Remarks
Maximum achievable SNR [bit]	$SNR_{y,max.bit}$	7.3	0.04	bit	

Table 11: Maximum achievable SNR [bit]

Item	Symbol	Typ.	Std. Dev.	Unit	Remarks
Maximum achievable SNR [dB]	$SNR_{y,max.dB}$	44.1	0.26	dB	

Table 12: Maximum achievable SNR [dB]

4.2.3 Dynamic Range

Dynamic range $DYN_{out.bit}$ in [bit].

$$DYN_{out} = \frac{\mu_{e.sat}}{\sigma_{d_0}} \quad (7)$$

$$DYN_{out.bit} = \log_2(DYN_{out}) \quad (8)$$

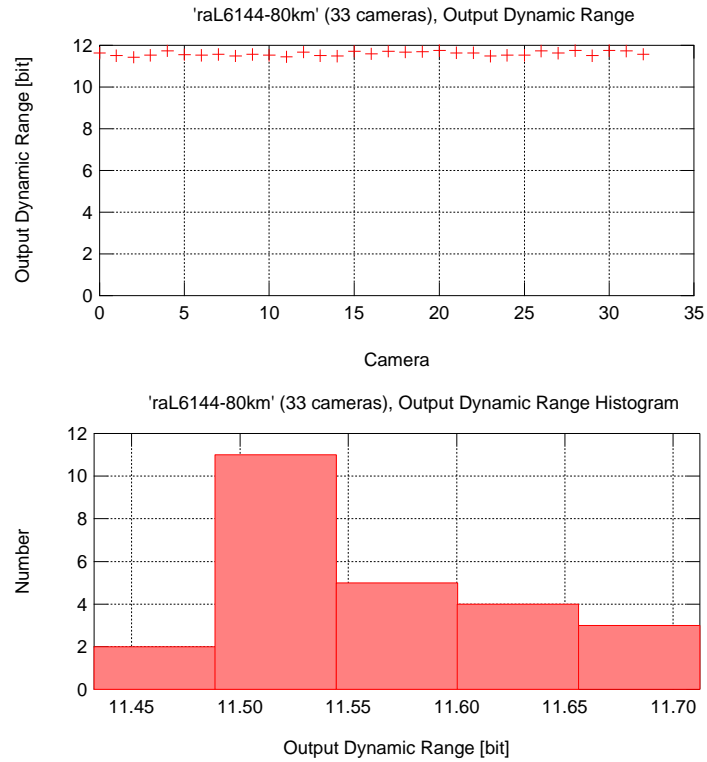


Figure 10: Output Dynamic Range

Item	Symbol	Typ.	Std. Dev.	Unit	Remarks
Output Dynamic Range	$DYN_{out.bit}$	11.6	0.10	bit	

Table 13: Output Dynamic Range

4.3 Raw Measurement Data

4.3.1 Mean Gray Value

Mean gray value $\mu_y(\mu_p)$ in [DN] is plotted versus number of photons μ_p in [p \sim] collected in a pixel during exposure time.

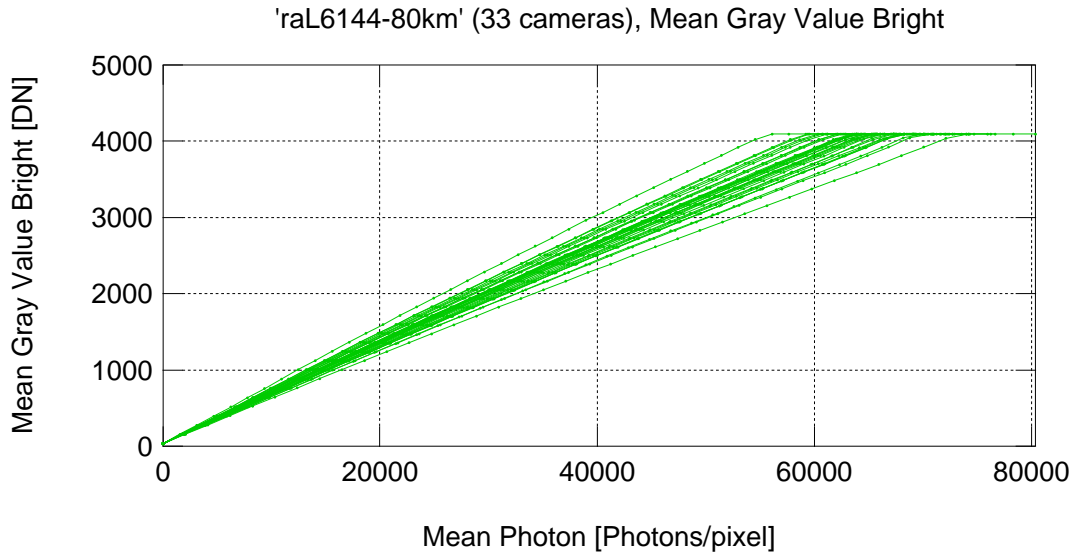


Figure 11: Mean Gray Values of the Cameras with Illuminated Pixels

4.3.2 Variance of the Temporal Distribution of Gray Values

The variance of the temporal distribution of gray values $\sigma_{y,temp}^2(\mu_p)$ in $[\text{DN}^2]$ is plotted versus number of photons μ_p in $[\tilde{p}]$ collected in a pixel during exposure time.

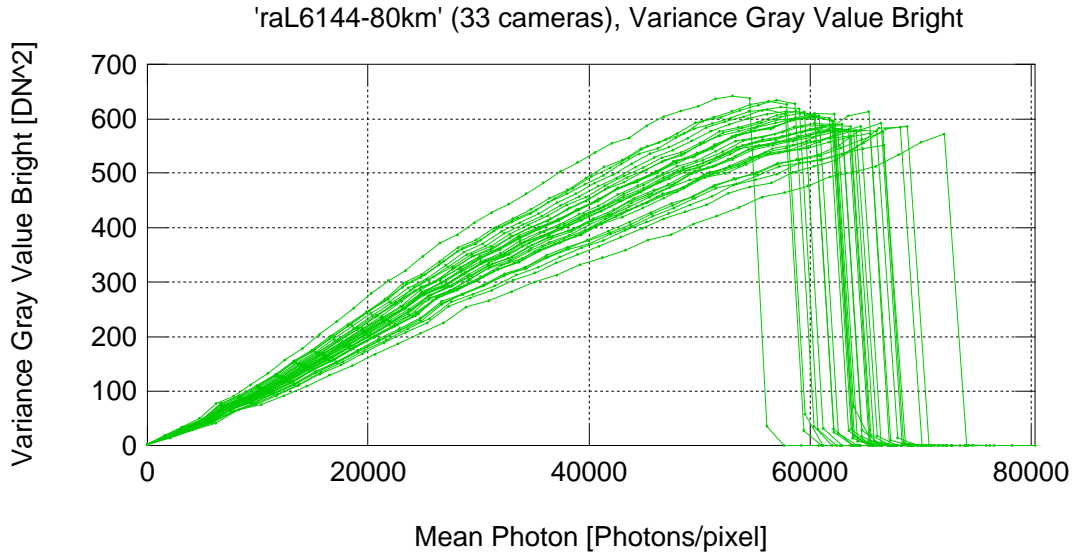


Figure 12: Variance Values for the Temporal Distribution of Gray Values with Illuminated Pixels

Saturation Capacity The saturation point is defined as the maximum of the curve in figure 12. The abscissa of the maximum point is the number of photons $\mu_{p.sat}$ where the camera saturates. The saturation capacity $\mu_{e.sat}$ in electrons is computed according to the mathematical model as:

$$\mu_{e.sat} = \eta \mu_{p.sat} \quad (9)$$

4.3.3 Mean of the Gray Values Dark Signal

Mean of the gray values dark signal $\mu_{y.dark}(T_{exp})$ in [DN] is plotted versus exposure time in [s].

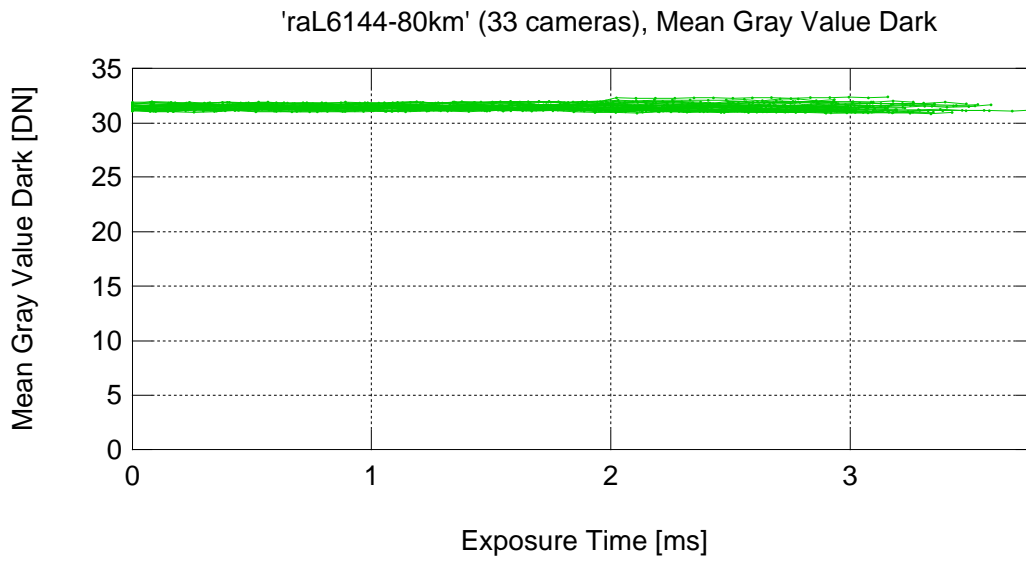


Figure 13: Mean Gray Values for the Cameras in Darkness

4.3.4 Variance of the Gray Value Temporal Distribution in Darkness

The variance of the temporal distribution of gray values in darkness $\sigma_{y.temp.dark}^2(T_{exp})$ in $[DN^2]$ is plotted versus exposure time T_{exp} in $[s]$.

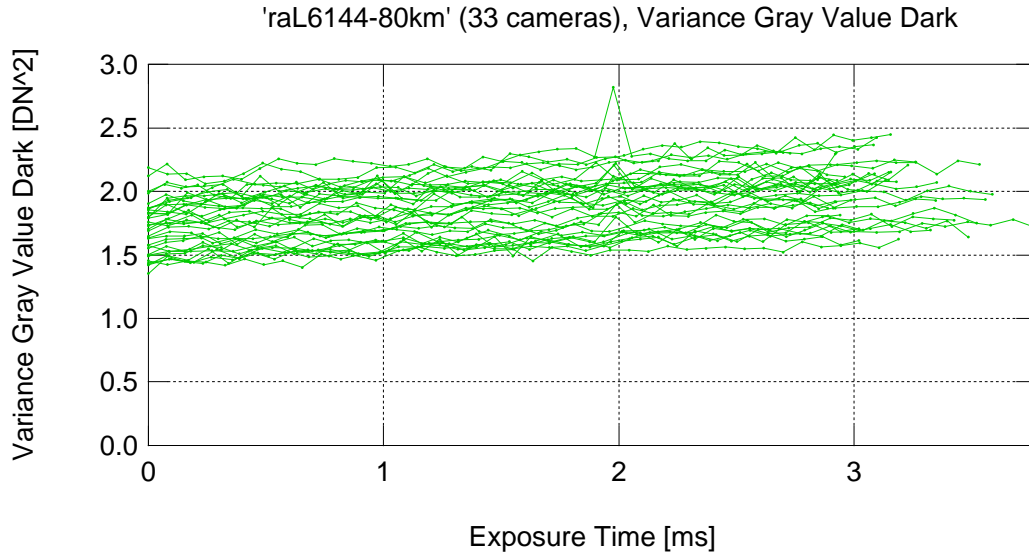


Figure 14: Variance Values for the Temporal Distribution of Gray Values in Darkness

Temporal Dark Noise The dark noise for exposure time zero is found as the offset of the linear correspondence in figure 14. Match a line (with offset) to the linear part of the data in the diagram. The dark noise for exposure time zero $\sigma_{d_0}^2$ is found as the offset of the line divided by the square of the overall system gain K .

$$\sigma_{d_0} = \sqrt{\frac{\sigma_{y.temp.dark}^2(T_{exp} = 0)}{K^2}} \quad (10)$$

4.3.5 Light Induced Variance of the Temporal Distribution of Gray Values

The light induced variance of the temporal distribution of gray values in $[\text{DN}^2]$ is plotted versus light induced mean gray value in $[\text{DN}]$.

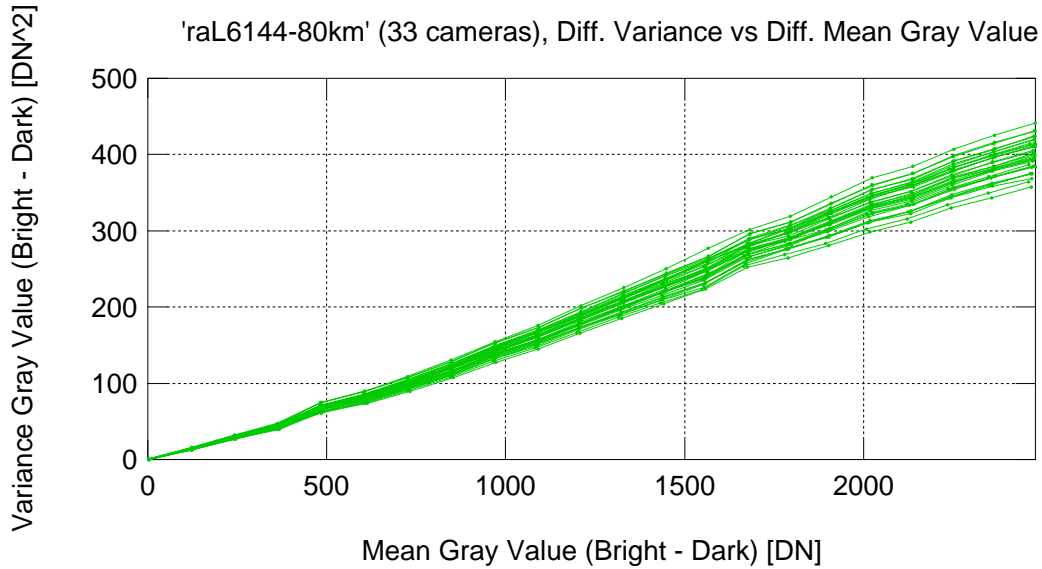


Figure 15: Light Induced Variance of the Temporal Distribution of Gray Values Versus Light Induced Mean Gray Value

Overall System Gain The overall system gain K is computed according to the mathematical model as:

$$K = \frac{\sigma_{y,temp}^2 - \sigma_{y,temp.dark}^2}{\mu_y - \mu_{y.dark}} \quad (11)$$

which describes the linear correspondence in figure 15. Match a line starting at the origin to the linear part of the data in this diagram. The slope of this line is the overall system gain K .

4.3.6 Light Induced Mean Gray Value

The light induced mean gray value $\mu_y - \mu_{y.dark}$ in [DN] is plotted versus the number of photons collected in a pixel during exposure time $K\mu_p$ in [p \sim].

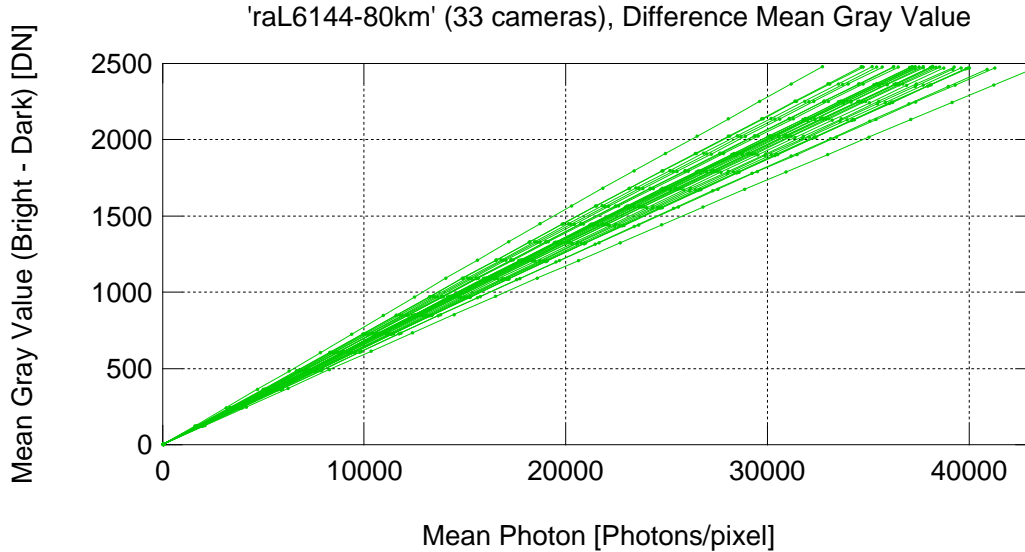


Figure 16: Light Induced Mean Gray Value Versus the Number of Photons

Total Quantum Efficiency The total quantum efficiency η is computed according to the mathematical model as:

$$\eta = \frac{\mu_y - \mu_{y.dark}}{K\mu_p} \quad (12)$$

which describes the linear correspondence in figure 16. Match a line starting at the origin to the linear part of the data in this diagram. The slope of this line divided by the overall system gain K yields the total quantum efficiency η .

The number of photons μ_p is calculated using the model for monochrome light. The number of photons Φ_p collected in the geometric pixel per unit exposure time [p \sim /s] is given by:

$$\Phi_p = \frac{EA\lambda}{hc} \quad (13)$$

with the irradiance E on the sensor surface [W/m²], the area A of the (geometrical) pixel [m²], the wavelength λ of light [m], the Planck's constant $h \approx 6.63 \cdot 10^{-34}$ Js, and the speed of light $c \approx 3 \cdot 10^8$ m/s. The number of photons can be calculated by:

$$\mu_p = \Phi_p T_{exp} \quad (14)$$

during the exposure time T_{exp} . Using equation 12 and the number of photons μ_p , the total quantum efficiency η can be calculated as:

$$\eta = \frac{hc}{AT_{exp}} \frac{1}{E} \frac{1}{\lambda} \frac{\mu_p - \mu_{y.dark}}{K} \quad (15)$$

4.3.7 Dark Current Versus Housing Temperature

The logarithm to the base 2 of the dark current in $[e^-/s]$ versus deviation of the housing temperature from 30°C in $[^\circ\text{C}]$

Not measured!

5 Characterizing Total and Spatial Noise

5.1 Basic Parameters

5.1.1 Spatial Offset Noise

Standard deviation of the spatial offset noise σ_o referenced to electrons in $[e^-]$.

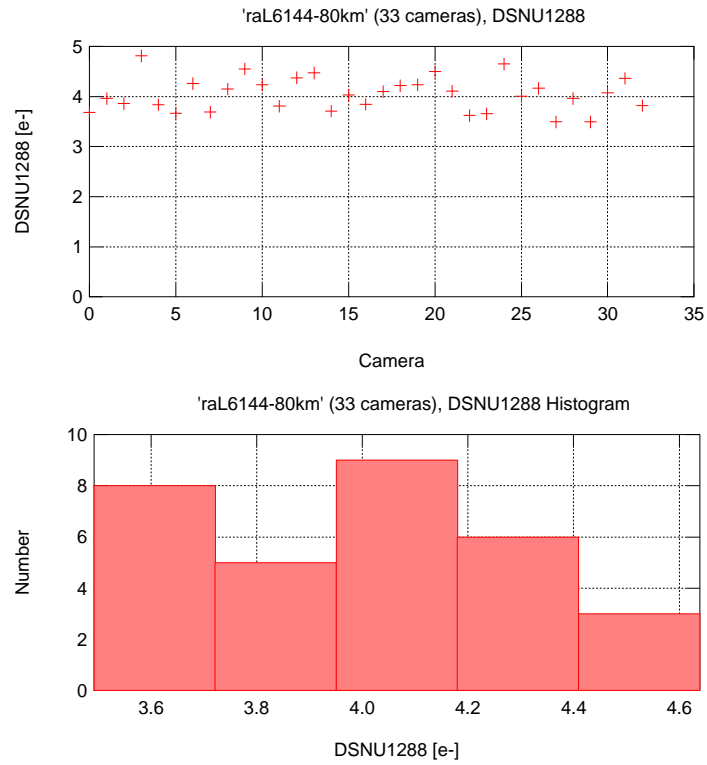


Figure 17: Spatial Offset Noise ($DSNU_{1288}$)

Item	Symbol	Typ.	Std. Dev.	Unit	Remarks
Spatial Offset Noise ($DSNU_{1288}$)	σ_o	4.0	0.3	e^-	

Table 14: Spatial Offset Noise ($DSNU_{1288}$)

5.1.2 Spatial Gain Noise ⁽⁴⁾

Standard deviation of the spatial gain noise S_g in [%].

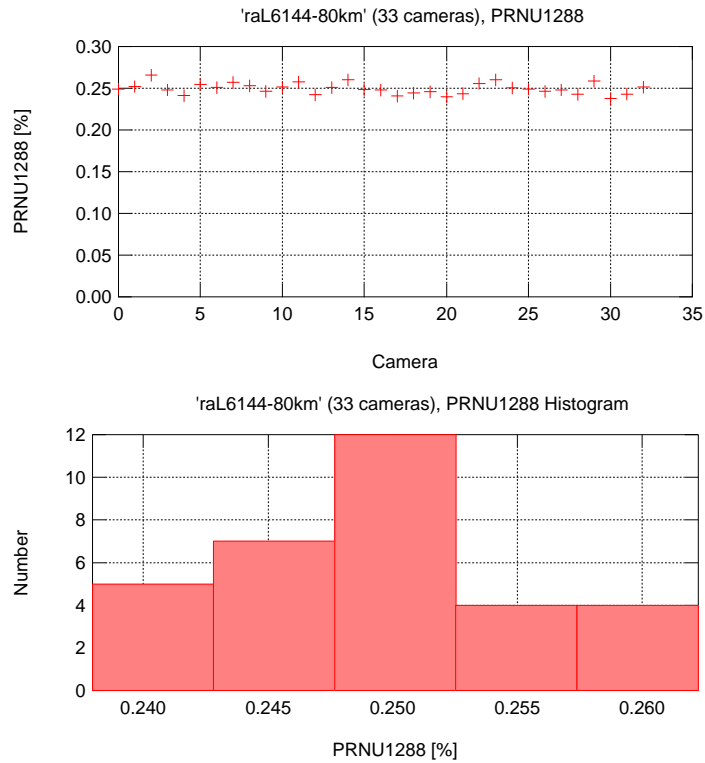


Figure 18: Spatial Gain Noise ($PRNU_{1288}$)

Item	Symbol	Typ.	Std. Dev.	Unit	Remarks
Spatial Gain Noise ($PRNU_{1288}$)	S_g	0.2	0.0	%	

Table 15: Spatial Gain Noise ($PRNU_{1288}$)

⁽⁴⁾ See appendix "Deviation in Quantum Efficiency" and "Photo Response Non Uniformity".

5.2 Raw Measurement Data

5.2.1 Standard Deviation of the Spatial Dark Noise

Standard deviation of the spatial dark noise in [DN] versus exposure time in [s] .

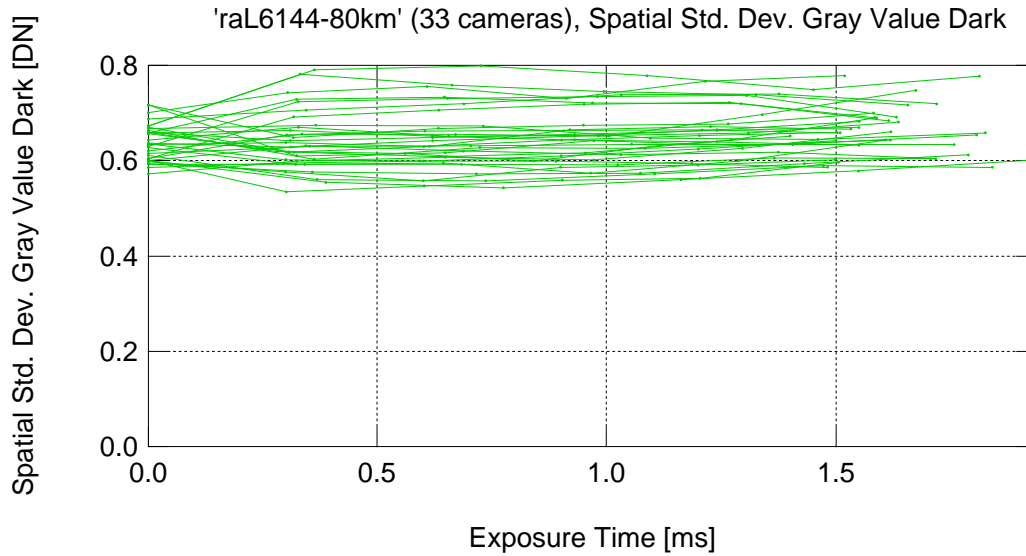


Figure 19: Standard Deviation of the Spatial Dark Noise

From the mathematical model, it follows that the **variance of the spatial offset noise** σ_o^2 should be constant and not dependent on the exposure time. Check that the data in the figure 19 forms a flat line. Compute the mean of the values in the diagram. The mean divided by the conversion gain K gives the standard deviation of the spatial offset noise σ_o .

$$\text{DSNU}_{1288} = \sigma_o = \frac{\sigma_{y.spat.dark}}{K} \quad (16)$$

The square of the result equals the variance of the spatial offset noise σ_o^2 .

5.2.2 Light Induced Standard Deviation of the Spatial Noise

Light induced standard deviation of the spatial noise in [DN] versus light induced mean of gray values [DN] .

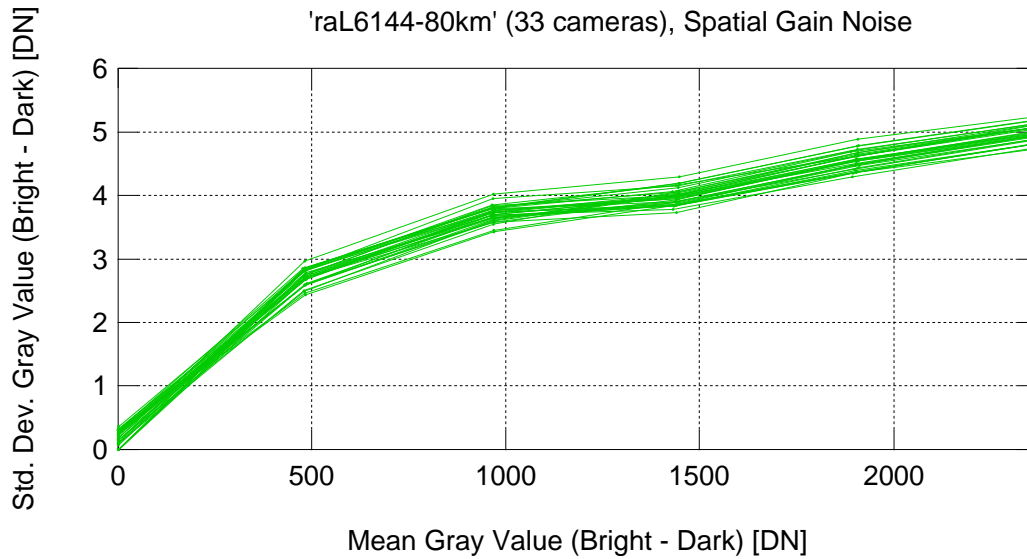


Figure 20: Light Induced Standard Deviation of the Spatial Noise

The **variance coefficient of the spatial gain noise** S_g^2 or its standard deviation value S_g respectively, is computed according to the mathematical model as:

$$\text{PRNU}_{1288} = S_g = \frac{\sqrt{\sigma_{y.spac}^2 - \sigma_{y.spac.dark}^2}}{\mu_y - \mu_{y.dark}}, \quad (17)$$

which describes the linear correspondence in figure 20. Match a line through the origin to the linear part of the data. The line's slope equals the standard deviation value of the spatial gain noise S_g .

References

- [1] EUROPEAN MACHINE VISION ASSOCIATION (EMVA): *EMVA Standard 1288 - Standard for Characterization and Presentation of Specification Data for Image Sensors and Cameras (Release A1.03)*. 2006

To whom it may concern

Ahrensburg, October 02, 2013

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Appendix

Measurement protocol - Basler racer Camera Series

1) Deviation in Quantum Efficiency

2) Photo Response Non Uniformity

Dear Sir or Madam,

Please note that the current EMVA Standard 1288 camera calculation model does not fit exactly the most recent technological advance as e.g. realized in the latest CMOS sensors.

The quantum efficiency information given in this camera measurement protocol was calculated assuming the current EMVA Standard 1288 regulations.

However, the quantum efficiency information (see below) reported by the sensor manufacturer for the sensors used in the Basler racer camera series differs from the quantum efficiency information given in this camera specification.

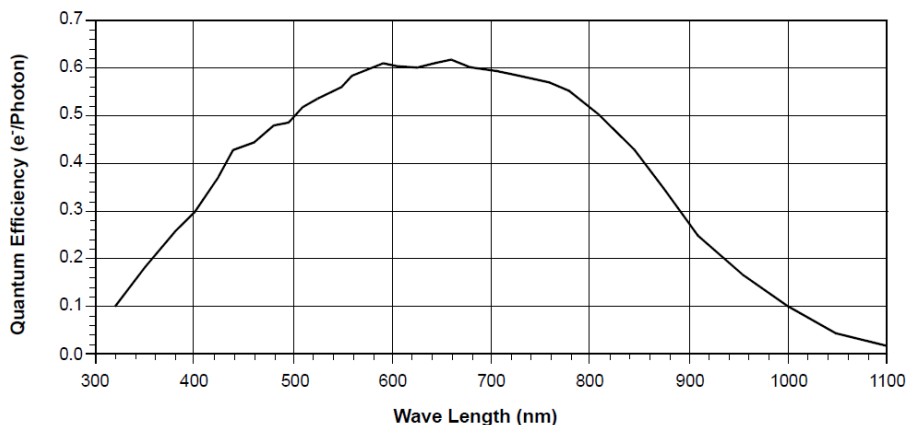


Fig. 1: Quantum Efficiency of the Monochrome Sensor in 12 Bit Depth Mode

Furthermore, please note that the Photo Response Non Uniformity (PRNU) information given in this report refers to the use of shading compensation for a specific operating point.

Independent evaluations of series cameras using the cameras default shading settings confirmed a PRNU of 0.5% on average.

Best regards



Marc Oliver Nehmke, Product Manager

